Vol. No.6, Issue No. 04, April 2017

www.ijarse.com



RESPONSE OF R C FRAME STRUCTURES RESTING ON RAFT FOUNDATION USING STAADPRO

Prof. Mahadevam, sindhu P², Venkatadri E³

¹Asst.professor, ^{2,3}UG Students

^{1,2,3}Department of civil engineering, Shri Pillappa College of Engineering, Bangalore

ABSTRACT

In the analysis of framed structure the base is considered to be fixed neglecting the effect of soil and foundation flexibility. Flexibility of the soil causes the decrease in stiffness resulting increase in the natural period of the structure. Such increase in the natural periods, changes the seismic response of structure hence it may be an important issue for design considerations. The present study provides systematic guidelines for determining the natural periods of frame buildings due to the effect of soil-flexibility and identification of spring stiffness for different regular and irregular story buildings and various influential parameters have identified and the effect of the same on change in natural periods has to be studied. The study has carried out for building with Isolated, mat and pile foundations for different soil conditions like soft, medium and hard strata, and a comparison between the regular and irregular buildings and natures of change in the natural periods has to be present. And response spectrum analysis this study may useful for seismic design. In the soil structure interaction analysis, the building frame, foundation and soil mass consider as a complete structure which is subjected to different types of loads like dead load, live load, wind load, seismic load etc. Seismic load is essential in case of multi-storey building. In the present work, the linear interaction analysis of a three-bay six -storey plane building is considered.

The investigation on the energy transfer mechanism from soils to buildings during earthquakes is critical for the design of earthquake resistant structures and for upgrading existing structures. Thus the need for research into Soil-Structure Interaction (SSI) problems is greater than ever. Moreover, recent studies show that the effects of SSI may be detrimental to the seismic response of structure and neglecting SSI in analysis may lead to unconservative design. Despite this, the conventional design procedure usually involves assumption of fixity at the base of foundation neglecting the flexibility of the foundation, the compressibility of soil mass and consequently the effect of foundation settlement on further redistribution of bending moment and shear force demands. Hence the soil-structure interaction analysis of multi-story buildings is the main focus of this study; the effects of SSI are analyzed for typical multi-story building resting on raft foundation. Three-dimensional FEM model is constructed to analyze the effects of different soil conditions and number of stories on the vibration characteristics and seismic response demands of building structures.

Keywords: Earthquake, Foundation, Soil Structure Interaction.

I. INTRODUCTION

Over the past 40 years, considerable progress has been made in understanding the nature of earthquakes and how they damage structures, and in improving the seismic performance of the built environment. However, much remains unknown regarding the prevention or mitigation of earthquake damage in worldwide, leaving room for further studies. During past and recent earthquakes, it is realized that the soil-structure interaction

Vol. No.6, Issue No. 04, April 2017 www.ijarse.com

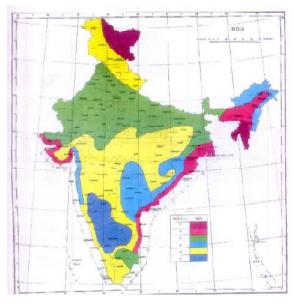


(SSI) effects play an important role in determining the behaviour of building structures. The experienced seismic excitation can be considered as function of the fault rupture mechanism, travel path effects, local site effects, and SSI effects. Irrespective of the structure, the local soil conditions can dramatically influence the earthquake motion from the bedrock level to the ground surface, through their dynamic filtering effects. One example is the 1985 Mexico City earthquake where deep soft soils amplified the ground motion and modified the frequency of ground shaking. Similar behaviour was observed during the 1989 Loma Prieta earthquake, in which the sections of the Cypress freeway in Oakland collapsed due to the soil-related motion amplification. The seismic soil structure interaction of multi-story buildings becomes very important after the destruction of recent major earthquakes. For the structure founded on the soil, the motion of the base of the structure will be different from the case of fixed base, because of the coupling of the structure-soil system. It is true that taking the soil into account when calculating the seismic response of the structure does complicate the analysis considerably. It also makes it necessary to estimate additional key parameters, which are difficult to determine, such as the dynamic properties of the soil such as site response, radiation damping and kinematic interaction. The soil structure interaction is a special field of analysis in earthquake engineering, this soil structure interaction is defined as "The dynamic interrelationship between the response of the structure is influenced by the motion of the soil and the soil response is influenced by the motion of structure is called a soil structure interaction." However engineering community discussed about SSI only when the basement motion by interaction force as compared to the ground motion of free field. The stress and deformation in the supporting soil cause vibration of structure generates base shear, moment, displacement and alter the natural period, since in reality it is not fixed base structure, the deformation of soil further modify the response of the structure. Any structure subjected to seismic force during an earthquake, the waves that arrive produce motions in the structure itself. Motions depend on the structures vibration characteristics and the structural layout or building. For the structure to response to the motion, it needs to overcome its own inertia, which result in an interaction between the structure and the soil. Such an interdependent behaviour between soil and structure regulating the overall response is referred as interaction behaviour in the present context. It is common practice that we consider the analysis of structure and foundation separately. The procedure in which the action of soil imparts the movement of the structure and the movement of the structure affects the action of the soil is called as SSI. Impendence difference is characterized as result of speed and thickness of soil. Seismic wave ventures quicker in hard shakes in contrasted with milder shakes and silt. As the waves goes from harder to milder rocks, they turn out to be moderate and should get greater in abundance to convey the same measure of the energy, in this way shaking tends to more grounded at sides with gentler surface layers, where seismic waves move more gradually.

Vol. No.6, Issue No. 04, April 2017 www.ijarse.com



II. EARTHQUAKE ZONES

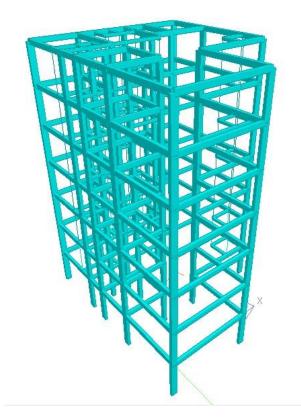




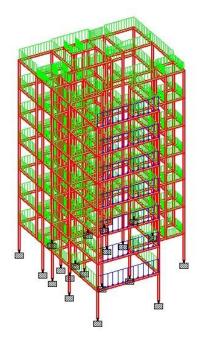
Vol. No.6, Issue No. 04, April 2017 www.ijarse.com



III. STAADPRO IMAGES



Render View



Load Distribution

Vol. No.6, Issue No. 04, April 2017

www.ijarse.com

IV. STAADPRO RESULTS AND DISCUSSION



```
STAAD.Pro V8i SELECTseries6
                                 Version 20.07.11.33
                                 Proprietary Program of
                                 Bentley Systems, Inc.
                                 Date= APR 2...
18:43:12
                                            APR 25, 2017
                          WSER ID:
INPUT FILE: C:\Users\user\Desktop\CONFARENCE replicate.STD
      2. START JOB INFORMATION
      3. ENGINEER DATE 25-APR-17
      4. END JOB INFORMATION
      5. INPUT WIDTH 79
      6. UNIT METER RN
      8. 1 0 0 0; 2 6.7 0 0; 3 0 0 -5.5; 4 3.6 0 -5.5; 5 0 0 -8.8; 6 3.6 0 -8.8
      7. JOINT COORDINATES
      9. 7 0 0 -10.6; 8 2 0 -8.8; 9 2 0 -10.6; 10 0 0 -11.8; 11 1.7 0 -10.6
     10. 12 1.7 0 -11.8; 13 2.8 0 -10.6; 14 2.8 0 -11.8; 15 0 0 -15.1; 17 3.6 0 -15.1
11. 18 3.6 0 -10.6; 19 7.6 0 -15.1; 20 7.6 0 -10.6; 21 6.2 0 -15.1; 22 5 0 -15.1
     12. 23 7.6 0 -13.6; 24 6.2 0 -13.6; 25 5 0 -13.6; 26 9.4 0 -15.1; 27 12.7 0 -15.1
13. 28 7.6 0 -11.5; 29 9.4 0 -11.5; 30 12.7 0 -11.5; 31 6.7 0 -5.5; 32 12.7 0 -5.3
     14. 33 10.7 0 -5.5; 34 12.7 0 -7.4; 35 10.7 0 -7.4; 36 0 -3 0; 37 6.7 -3 0
          38 0 -3 -5.5; 39 3.6 -3 -5.5; 40 0 -3 -8.8; 41 3.6 -3 -8.8; 42 0 -3 -10.6
     16. 43 2 -3 -8.8; 44 2 -3 -10.6; 50 0 -3 -15.1; 51 3.6 -3 -15.1; 52 3.6 -3 -10.6
     17. 53 7.6 -3 -15.1; 60 9.4 -3 -15.1; 61 12.7 -3 -15.1; 62 7.6 -3 -11.5

18. 63 9.4 -3 -11.5; 64 12.7 -3 -11.5; 65 6.7 -3 -5.5; 66 12.7 -3 -5.5; 67 0 1 0

19. 68 6.7 3 0; 69 0 3 -5.5; 70 3.6 3 -5.5; 71 0 3 -8.8; 72 3.6 3 -8.8
```

```
--- PAGE 1 Ends Here >-
STAAD SPACE
                                                                            PAGE NO.
39. 159 9.4 9 -15.1; 160 12.7 9 -15.1; 161 7.6 9 -11.5; 162 9.4 9 -11.5
40. 163 12.7 9 -11.5; 164 6.7 9 -5.5; 165 12.7 9 -5.5; 166 10.7 9 -5.5
41. 167 12.7 9 -7.4; 168 10.7 9 -7.4; 169 0 12 0; 170 6.7 12 0; 171 0 12 -5.5
42. 172 3.6 12 -5.5; 173 0 12 -8.8; 174 3.6 12 -8.8; 175 0 12 -10.6; 176 2 12 -8.8
43. 177 2 12 -10.6; 178 0 12 -11.8; 179 1.7 12 -10.6; 180 1.7 12 -11.8
44. 181 2.8 12 -10.6; 182 2.8 12 -11.8; 183 0 12 -15.1; 184 3.6 12 -15.1
45. 185 3.6 12 -10.6; 186 7.6 12 -15.1; 187 7.6 12 -10.6; 188 6.2 12 -15.1
46. 189 5 12 -15.1; 190 7.6 12 -13.6; 191 6.2 12 -13.6; 192 5 12 -13.6
47, 193 9,4 12 -15.1; 194 12.7 12 -15.1; 195 7.6 12 -11.5; 196 9,4 12 -11.5
48. 197 12.7 12 -11.5; 198 6.7 12 -5.5; 199 12.7 12 -5.5; 200 10.7 12 -5.5
49. 201 12.7 12 -7.4; 202 10.7 12 -7.4; 203 0 15 0; 204 6.7 15 0; 205 0 15 -5.5
50. 206 3.6 15 -5.5; 207 0 15 -8.8; 208 3.6 15 -8.8; 209 0 15 -10.6; 210 2 15 -8.8
51. 211 2 15 -10.6; 212 0 15 -11.8; 213 1.7 15 -10.6; 214 1.7 15 -11.8
52. 215 2.8 15 -10.6; 216 2.8 15 -11.8; 217 0 15 -15.1; 218 3.6 15 -15.1
53. 219 3.6 15 -10.6; 220 7.6 15 -15.1; 221 7.6 15 -10.6; 222 6.2 15 -15.1
54. 223 5 15 -15.1; 224 7.6 15 -13.6; 225 6.2 15 -13.6; 226 5 15 -13.6
55. 227 9.4 15 -15.1; 228 12.7 15 -15.1; 229 7.6 15 -11.5; 230 9.4 15 -11.5
56. 231 12.7 15 -11.5; 232 6.7 15 -5.5; 233 12.7 15 -5.5; 234 10.7 15 -5.5
57. 235 12.7 15 -7.4; 236 10.7 15 -7.4; 237 0 18 0; 238 6.7 18 0; 239 0 18 -5.5
58. 240 3.6 18 -5.5; 241 0 18 -8.8; 242 3.6 18 -8.8; 243 0 18 -10.6; 244 2 18 -8.8
59. 245 2 18 -10.6; 246 0 18 -11.8; 247 1.7 18 -10.6; 248 1.7 18 -11.8
60. 249 2.8 18 -10.6; 250 2.8 18 -11.8; 251 0 18 -15.1; 252 3.6 18 -15.1
61. 253 3.6 18 -10.6; 254 7.6 18 -15.1; 255 7.6 18 -10.6; 256 6.2 18 -15.1
62, 257 5 18 -15.1; 258 7.6 18 -13.6; 259 6.2 18 -13.6; 260 5 18 -13.6
63. 261 9.4 18 -15.1; 262 12.7 18 -15.1; 263 7.6 18 -13.5; 264 5.4 18 -11.5
64. 265 12.7 18 -11.5; 266 6.7 18 -5.5; 267 12.7 18 -5.5; 268 10.7 18 -5.5
65. 269 12.7 18 -7.4; 270 10.7 18 -7.4
     MEMBER INCIDENCES
1 2 1; 2 1 3; 3 3 4; 4 4 6; 5 6 8; 6 8 5; 7 3 5; 8 5 7; 9 7 10; 10 10 15
66. MEMBER INCIDENCES
68. 11 15 17; 13 7 11; 14 11 9; 15 8 9; 16 9 13; 17 13 14; 18 14 12; 19 12 11 69. 20 12 10; 21 13 18; 22 18 17; 23 17 22; 24 19 23; 25 18 20; 26 21 19; 27 22 21
70. 28 23 28; 29 25 22; 30 24 21; 31 25 24; 32 23 24; 33 28 20; 34 28 29; 35 30 29
71. 36 19 26; 37 26 29; 38 30 27; 39 26 27; 40 2 31; 41 31 35; 42 32 34; 43 33 32 72. 44 34 30; 45 33 35; 46 34 35; 47 15 50; 49 7 42; 50 5 40; 51 3 38; 52 1 36 73. 53 2 37; 54 31 65; 55 4 39; 56 6 41; 57 8 43; 58 18 52; 59 17 51; 61 9 44
```

Vol. No.6, Issue No. 04, April 2017

www.ijarse.com



```
66. MEMBER INCIDENCES
67. 1 2 1; 2 1 3; 3 3 4; 4 4 6; 5 6 8; 6 8 5; 7 3 5; 8 5 7; 9 7 10; 10 15
68. 11 15 17; 13 7 11; 14 11 9; 15 8 9; 16 9 13; 17 13 14; 18 14 12; 19 12 11
69. 20 12 10; 21 13 18; 22 18 17; 23 17 22; 24 19 23; 25 18 20; 26 21 19; 27 22 21
70. 28 23 28; 29 25 22; 30 24 21; 31 25 24; 32 23 24; 33 28 20; 34 28 29; 35 30 29
71. 36 19 26; 37 26 29; 38 30 27; 39 26 27; 40 2 31; 41 31 33; 42 32 34; 43 33 32
72. 44 34 30; 45 33 35; 46 34 35; 47 15 50; 49 7 42; 50 5 40; 51 3 38; 52 1 36
73. 53 2 37; 54 31 65; 55 4 39; 56 6 41; 57 8 43; 58 18 52; 59 17 51; 61 9 44
74. 65 19 53; 68 28 62; 70 29 63; 71 27 61; 72 26 60; 73 30 64; 77 32 66; 78 1 67
75. 79 2 68; 80 3 69; 81 4 70; 82 5 71; 83 6 72; 84 7 73; 85 8 74; 86 9 75
76. 87 10 76; 88 11 77; 89 12 78; 90 13 79; 91 14 80; 92 15 81; 93 17 82; 94 18 83
77. 95 19 84; 96 20 85; 97 21 86; 98 22 87; 99 23 88; 100 24 89; 101 25 90
78. 102 26 91; 103 27 92; 104 28 93; 105 29 94; 106 30 95; 107 31 96; 108 32 97
79. 109 33 98; 110 34 99; 111 35 100; 112 68 67; 113 67 69; 114 69 70; 115 70 72
80. 116 72 74; 117 74 71; 118 69 71; 119 71 73; 120 73 76; 121 76 81; 122 81 82 81. 123 73 77; 124 77 75; 125 74 75; 126 75 79; 127 79 80; 128 80 78; 129 78 77
 82. 130 78 76; 131 79 83; 132 83 82; 133 82 87; 134 84 88; 135 83 85; 136 86 84
 83, 137 87 86; 138 88 93; 139 90 87; 140 89 86; 141 90 89; 142 88 89; 143 93 85
      144 93 94; 145 95 94; 146 84 91; 147 91 94; 148 95 92; 149 91 92; 150 68 96
 85. 151 96 98; 152 97 99; 153 98 97; 154 99 95; 155 98 100; 156 99 100; 157 67 101
 86. 158 68 102; 159 69 103; 160 70 104; 161 71 105; 162 72 106; 163 73
 37. 164 74 108; 165 75 109; 166 76 110; 167 77 111; 168 78 112; 169 79 113
 88. 170 80 114; 171 81 115; 172 82 116; 173 83 117; 174 84 118; 175 85 119
 89. 176 86 120; 177 87 121; 178 88 122; 179 89 123; 180 90 124; 181 91 125
90. 182 92 126; 183 93 127; 184 94 128; 185 95 129; 186 96 130; 187 97 131
  91. 188 98 132; 189 99 133; 190 100 134; 191 102 101; 192 101 103; 193 103 104
 91. 188 98 132; 189 99 133; 190 100 134; 191 102 101; 192 101 103; 193 103 104 92. 194 104 106; 195 106 108; 196 108 105; 157 103 105; 198 105 107; 199 107 110 93. 200 110 115; 201 115 116; 202 107 111; 203 111 109; 204 108 109; 205 109 113 94. 206 113 114; 207 114 112; 208 112 111; 209 113 110; 210 113 117; 211 117 116
                                          PAGE 2 Ends Here
  95. 212 116 121; 213 118 122; 214 117 119; 215 120 118; 216 121 120; 217 122 127 96, 218 124 121; 219 123 120; 220 124 123; 221 122 123; 222 127 119; 223 127 128 97, 224 129 128; 225 118 128; 226 125 128; 227 128 126; 228 125 126; 229 102 130
 98. 280 130 132; 231 131 133; 232 132 131; 233 133 125; 234 132 134; 235 133 134 39. 236 115 81; 237 107 73; 238 105 71; 239 103 69; 240 101 67; 241 102 68 100, 242 130 96; 243 104 70; 244 106 72; 245 108 74; 246 117 83; 247 116 82
```

```
- PAGE NO.
 STAAD SPACE
151. 548 230 196; 549 228 194; 550 227 193; 551 231 197; 552 233 199; 553 203 237 152. 554 204 238; 555 205 239; 556 206 240; 557 207 241; 558 208 242; 359 209 243
153. 560 210 244; 561 211 245; 562 212 246; 563 213 247; 564 214 248; 565 215 249
154. 566 216 250; 567 217 251; 568 218 252; 569 219 253; 570 220 254; 571 221 255
155. 572 222 256; 573 223 257; 574 224 258; 575 225 259; 576 226 260; 577 227 261
156. 578 228 262; 579 229 263; 580 230 264; 581 231 265; 582 232 266; 583 233 267
157. 584 234 268; 585 235 269; 586 236 270; 587 238 237; 588 237 239; 589 239
158. 590 240 242; 591 242 244; 592 244 241; 593 239 241; 594 241 243; 595 243 246
159. 596 246 251; 597 251 252; 598 243 247; 599 247 245; 600 244 245; 601 245 249
160. 602 249 250; 603 250 248; 604 248 247; 605 248 246; 606 249 253; 607 253 252
161. 608 252 257; 609 254 258; 610 253 255; 611 256 254; 612 257 256; 613 258 263
162. 614 260 257; 615 259 256; 616 260 259; 617 258 259; 618 263 255; 619 263 264
163. 620 265 264; 621 254 261; 622 261 264; 623 265 262; 624 261 262; 625 238
164 - 626 266 268; 627 267 269; 628 268 267; 629 269 265; 630 268 270; 631 269 270
165. 632 251 217; 633 243 209; 634 241 207; 635 239 205; 636 237 203; 637 238 204
166. 638 266 232; 639 240 206; 640 242 208; 641 244 210; 642 253 219; 643 252
167. 644 245 211; 645 254 220; 646 263 229; 647 264 230; 648 262 228; 649 261 227
168. 650 265 231; 651 267 233
169. DEFINE MATERIAL START
170. ISOTROPIC CONCRETE
171. E 2.17185E+007
172. POISSON 0.17
173. DENSITY 23.5616
174. ALPHA 1E-005
175. DAMP 0.05
176. TYPE CONCRETE
177. G 9.28139E+006
                                                        De
178. TYPE CONCRETE
179. STRENGTH FCU 28500
180. STRENGTH FCU 27579
181. END DEFINE MATERIAL
183. 47 49 TO 54 59 65 71 72 77 TO 79 92 103 108 236 240 241 252 255 335 339 340 -
184. 351 354 434 438 439 450 453 533 537 538 549 552 632 636 637 648 -
185. 651 PRIS YD 0.45 ZD 0.2
```

Vol. No.6, Issue No. 04, April 2017

www.ijarse.com

IJARSE ISSN (O) 2319 - 8354 ISSN (P) 2319 - 8346

```
186. 1 TO 11 22 TO 24 26 TO 28 33 TO 44 112 TO 122 132 TO 134 136 TO 138 187. 143 TO 154 191 TO 201 211 TO 213 215 TO 217 222 TO 233 290 TO 300 - 188. 310 TO 312 314 TO 316 321 TO 332 389 TO 399 409 TO 411 413 TO 415 - 189. 420 TO 431 488 TO 498 508 TO 510 512 TO 514 519 TO 530 587 TO 597 - 190. 607 TO 609 611 TO 613 618 TO 629 PRIS YD 0.35 2D 0.2 191. 55 TO 58 61 68 70 81 83 85 86 94 104 105 243 TO 246 248 250 251 342 TO 345 - 192. 347 349 350 441 TO 444 446 448 449 540 TO 543 545 547 548 639 TO 642 644 - 193. 646 647 PRIS YD 0.3 ZD 0.3 194. 49 TO 51 54 59 65 72 73 80 82 84 93 95 102 106 107 237 TO 239 242 247 249 - 195. 253 254 336 TO 338 341 346 348 352 353 435 TO 437 440 445 447 451 452 534 - 196. S35 TO 536 539 544 546 550 551 633 TO 635 638 643 645 649 - 197. 650 PRIS YD 0.2 ZD 0.45
```

```
198. 13 14 16 TO 21 25 29 TO 32 45 46 123 124 126 TO 131 135 139 TO 142 155 156 -
199. 202 203 205 TO 210 214 218 TO 221 234 235 301 $2 304 TO 309 313 317 TO 320 -
199. 202 203 334 400 401 403 TO 408 412 416 TO 419 432 433 499 500 502 TO 507 511 -
200. 333 334 400 401 403 TO 408 412 416 TO 616 610 614 TO 617 630 -
201. 515 TO 518 531 532 598 599 601 TO 606 610 614 TO 617 630 -
202. 631 PRIS YD 0.2 ZD 0.2
203. CONSTANTS
204. E 25000 MEMB 15 87 TO 91 96 TO 101 109 TO 111 125 157 TO 190 204 256 TO 289 -
205. 303 355 TO 388 402 454 TO 487 501 553 TO 586 600
206. E CONCRETE MEMB 15 87 TO 91 96 TO 101 109 TO 111 125 157 TO 190 204 -
```

V. CONCLUSION

The paper shows that including soil in a model of structure does not always have beneficial effects, as often believed.

- 1. Designing using Software's like Staad reduces lot of time in design work.
- 2. Details of each and every member can be obtained using staad pro.
- 3. All the List of failed beams can be obtained and also Better Section is given by the software.
- 4. Accuracy is improved by using software.

The main aim of this report is to study how to approach the design of building based on IS codes. The loadings to be considered, planning of column, beam and slabs, analysis of building with the staad pro software.

1) Fundamental natural period

The fundamental natural period of a specific structure considering interaction is more than that of non-interaction investigation furthermore it increments as the shear modulus of the soil declines. With expansion in number of stories fundamental natural period increments.

2) Base shear

Base shear values for interaction case is more than that of non-interaction case, as the shear modulus of the soil abatements base shear increments. With expansion in number of stories base shear increments.

3) Maximum lateral displacement

For the increment in shear modulus and number of stories the maximum lateral displacement of the structural element discovered to be expanded. The estimations of maximum lateral displacement resulting from a fixed base analysis are impressively improved when interaction analysis of the system is considered.

Vol. No.6, Issue No. 04, April 2017

www.ijarse.com

REFERANCE

- [1.] Soil structure interaction effects on seismic response on multi-storied buildings on raft foundation. By, SHEHATA .E ABDEL RAHEEM.
- [2.] Studies on soil structure interaction of multi-storeyed buildings with rigid and flexible foundation. By, R.M.JENIFER PRIYANKA.
- [3.] Effects of soil structure interaction in seismic response of building resting on elevated surface. By,PROF. L.R. WANKHADE.
- [4.] Soil structure interaction effect on dynamic behaviour of 3D building frames with raft footing. By, KULADEEPU .M.
- [5.] Linear soil structure interaction analysis of the column of an unsymmetrical plane frame under seismic loading.
 - By, ANKUR ACHARYA.
- [6.] Soil structure interaction of framed structure supported on different types of foundation. By, Mr. K.G.Subramanya.
- [7.] Effects of soil structure interaction on the seismic response of existing RC frame building. By, M. JAWAD AREFI.
- [8.] Soil structure interaction analysis on a RC building with raft foundation under clayey soil condition. By, M. ROOPA.
- [9.] Parametric study of soil structure interaction of raft foundation by using dynamic analysis. By, MOHAMMED ZUBAIR.

BIOGRAPHICAL NOTES



Prof. Mahadeva M is working as assistant professor in civil engineering department for last 2 years and he also worked as assistant professor in k s institute of technology. He received is **M.Tech in civil engineering** with specialization in **CAD structures** from visvesvaraya technological university. His research interest is in the field of soil structure interaction, structural engineering, earth quake engineering.



U G STUDENTS
SINDHU P
VENKATADRI E



ISSN (P) 2319 - 8346